

**FOAM-FORMING PROPERTIES OF *Ilex paraguariensis* (MATE) SAPONIN: FOAMABILITY AND FOAM LIFETIME ANALYSIS BY WEIBULL EQUATION****Janine Treter, Maria P. G. Peixoto e George G. Ortega\***

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Saponins are natural soaplike foam-forming compounds widely used in foods, cosmetic and pharmaceutical preparations. In this work foamability and foam lifetime of foams obtained from *Ilex paraguariensis* unripe fruits were analyzed. Polysorbate 80 and sodium dodecyl sulfate were used as reference surfactants. Aiming a better data understanding a linearized 4-parameters Weibull function was proposed. The mate hydroethanolic extract (ME) and a mate saponin enriched fraction (MSF) afforded foamability and foam lifetime comparable to the synthetic surfactants. The linearization of the Weibull equation allowed the statistical comparison of foam decay curves, improving former mathematical approaches.

Keywords: saponin; *Ilex paraguariensis*; foam stability.

**INTRODUCTION**

*Ilex paraguariensis* A. St. Hil (Aquifoliaceae) is a native South American tree, widely known for its stimulant activity on the central nervous system and the production of erva-mate, a leaves coarse powder traditionally used in the preparation of stimulant tea-like beverages.<sup>1</sup> Mate is often associated with the high content of methylxanthines in leaves, but its saponin richness is seldom related. The occurrence, isolation and identification of the main saponins from mate leaves and fruits are well described in literature.<sup>2-9</sup> Mate saponins occur almost as bidesmosidic glycosides derived from oleanolic and ursolic acids having one or two sugar chains attached at the C-3 and C-28.<sup>5</sup>

Alike other saponins from superior plants (e.g. Quillaja, Gypsophila, Phytolacca and Polygala saponins), bacteria and marine animals, mate saponins are biodegradable hydrophilic surfactants.<sup>10-13</sup> Mate saponins are weakly hemolytic, non-irritating in the Draize topical test and they are also able to form abundant and persistent foam.<sup>14</sup>

Foamability is a desirable property required in some chemical, foods, cosmetic and pharmaceutical processes.<sup>15-19</sup> An ideal foam-forming must be non-toxic and able to produce abundant, dense and stable foam, even at low concentration.<sup>20,21</sup> There are several methods to assess foamability and foam stability,<sup>16,22</sup> including the foam decay evaluation and rate of liquid drained from foam. An extensive comparison among official and non-official methods for beer analysis was reported recently.<sup>22,23</sup> However, the data analysis of foam decay is still based on the logarithmic representation of the foam column height or the volume of liquid drainage versus time, notwithstanding it can lead to unreliable results and lack of fit.<sup>20,22</sup> This work aims, therefore, to study foam-forming properties of *Ilex paraguariensis* saponins, comparing foam lifetime, foamability and film drainage behavior against the reference surfactants sodium dodecyl sulfate and polysorbate 80. In the same context, an empirical linearization of the 4-parameters Weibull is proposed in order to compare the different foam profiles.

**EXPERIMENTAL****Materials**

The surfactants sodium dodecyl sulfate and polysorbate 80 were purchased from Merck. Unripe fruits of *Ilex paraguariensis* were kindly supplied by Barão Ervas e Chás, Cotegipe RS, Brazil. The test solutions were prepared using freshly obtained distilled water (conductivity of 2.8  $\mu\text{S}/\text{cm}$ ). The concentration of each test solution was equivalent to 10-fold the critical micellar concentration (cmc), namely mate extract (ME) 1.1  $\text{mmol L}^{-1}$ , enriched saponin fraction (MSF) 1.5  $\text{mmol L}^{-1}$ , polysorbate 80 (POL) 6.0  $\text{mmol L}^{-1}$  and sodium dodecyl sulfate (SDS) (85.8  $\text{mmol L}^{-1}$ ). The cmc of ME and MSF was calculated and expressed using matesaponin-I as saponin reference (mol. weight 996.45).<sup>14</sup>

**Preparation of the mate extract**

Fruits were manually separated from leaves and stalks, dried at 35 °C during 72 h in a air-forced oven (Memmert, Germany) and milled with a cutter mill (Retsch SK1, Germany). The plant powder (0.85  $\mu\text{m}$ ) was firstly macerated with an 40% ethanol solution (100 g/L) by 40 min and extracted by turbolyses (IKA T-25, Germany) during 15 min avoiding overheating. The extract was filtered and concentrated to one-half of its original volume in a rotary vacuum evaporator (Büchi B-480, USA) and immediately lyophilized thereafter (Modulyo 4L Edwards, USA).

The enriched saponin fraction was obtained by solid phase extraction and afterward lyophilized (Bras. Pat. PI 0501510-3 04/22/2005). The product is free of pigments, chlorophyll, flavonoids, polyphenols with very low electrolytes content.<sup>24</sup>

**Foamability and foam stability test**

A 20 mL sample of each surfactant solution was poured into a cylindrical glass column (35.5 x 3.6 cm) provided with a sinterized glass septum (G4, 3.6 cm x 4 mm) fixed at the column bottom. Dried

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compressed air was supplied by a reciprocal pump (Inalar compact, Brazil) at a flow rate of 2 L/min (Fluxometer Protec, Brazil) during exactly 20 s. Pipes and air purge valves internal diameters were 2 mm. The temperature was  $25 \pm 2$  °C (Figure 1).

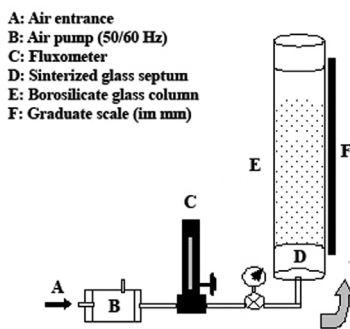


Figure 1. Instrumental device applied on foamability and foam stability test

The foam column height (foamability) was recorded immediately after air supply suppression. The volume of liquid drained (LVF) after 0; 1; 2; 3; 4; 5; 10; 30 and 60 min was measured using a graduated scale fixed onto the column considering the relationship between initial volume and its corresponding height as depicted on Figure 2.

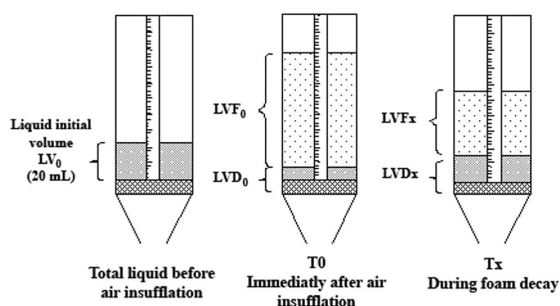


Figure 2. Schematic diagram from foam column. LVF: liquid volume fraction in foam; LVD: Liquid volume drained from foam

The liquid volume fraction in foam (LVF) was calculated by subtraction of the volume of liquid drained from 20, the total volume of the surfactant solution added in to the column (Equation 1).

$$LVF = 20 - LV \quad (1)$$

### Mathematical analysis

The liquid volume fraction in foam data were plotted against time and the curve equation calculated by the least squares method regression using the 4-parameters Weibull equation (Equation 2). Weibull coefficients alpha ( $\alpha$ ), beta ( $\beta$ ), gamma ( $\gamma$ ) and eta ( $\eta$ ), as well as regression standard deviation were calculated using Curve Expert 1.3 software. After the empirical linearization of the Weibull function (Equations 3 and 4), the intercept and slope calculated by the least squares method were compared by means of one-tail T test (P 0.05) for intercept (Equation 5) and slope (Equation 6)<sup>25</sup> using Excel 2003 software.

$$y = \alpha - \eta * \exp(-\gamma * x^\beta) \quad (2)$$

$$\ln[-\ln(\alpha - y)] = \beta \ln(x - \gamma) - \ln \eta \quad (3)$$

$$\ln(x) = -\beta \ln(\gamma) - \beta [\ln(x) / \ln(\eta)] \quad (4)$$

$$S(a) = \frac{SQE(1) + SQE(2)}{n_1 + n_2 - 4} * x \left[ \frac{1}{n_1} + \frac{1}{n_2} + \frac{\bar{x}_1}{S_{xx}^1} + \frac{\bar{x}_2}{S_{xx}^2} \right] \quad (5)$$

$$S(b) = \frac{SQE(1) + SQE(2)}{n_1 + n_2 - 4} * x \left[ \frac{1}{S_{xx}^1} + \frac{1}{S_{xx}^2} \right] \quad (6)$$

where:  $SQE$  is the regression standard deviation,  $S_{xx} = \sum(x_i - \bar{x})^2$ , and  $n$  the sample size.

## RESULTS AND DISCUSSION

Saponins are natural compounds able to yield abundant foam in aqueous solutions and several of them are profusely cited in the literature.<sup>26-28</sup> Nonetheless, mate saponins foamability is seldom mentioned and no precedent analytical studies about its foam-forming properties are related as far as we know.

A full evaluation of the foam column height decay was impracticable owing the irregular breakdown patterns observed within a same working solution. Thus, the foam decay was analyzed indirectly by measuring the liquid volume drained from foam (LVD).

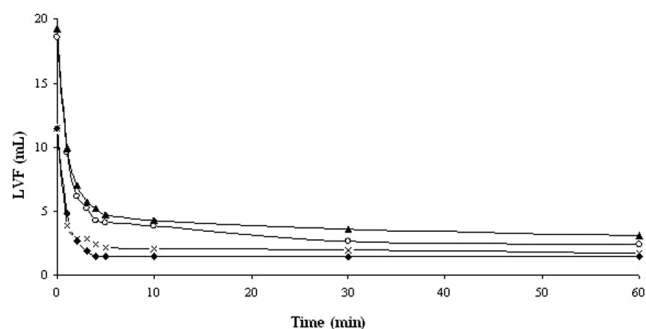
The foam stability and foamability data of mate extract (ME), enriched saponin fraction (MSF), polysorbate 80 (POL) and sodium dodecyl sulfate (SDS) are described in Table 1. The foamability of ME and MSF was comparable to POL and SDS ones. Foamability of ME was slightly lower than MSF, probably as a result of the presence of other compounds on the total extract. On the contrary, foams from ME and MSF stood longer and were still evident after 60 min, unlike POL and SDS, where the foam collapse was nearly complete. The decay rate of the LVF was higher and more intense in SDS and POL foams than in ME and MSF ones (Table 1, Figure 3). At the process beginning, the first confidence limits of the mean LVF values overlap and therefore no statistical relationship between liquid drainage rate and foam stability could be established. Only at the end of the experiment the LVF values of ME and MSF ( $2.38 \pm 0.09$  and  $3.05 \pm 0.14$  mL, respectively) became significantly higher than POL ( $1.71 \pm 0.04$  mL) and SDS ( $1.43 \pm 0.05$  mL) values.

Table 1. Determination of LVF values and foamability for ME, MSF, POL and SDS ( $25 \pm 2$  °C)

Time (min)	LVF (mL)			
	ME	MSF	POL	SDS
0	18.57 (14.5) <sup>a</sup>	19.24 (16.7) <sup>a</sup>	11.43 (14.5) <sup>a</sup>	11.43 (17.2) <sup>a</sup>
1	9.52	9.90	3.81	4.76
2	6.19	7.05	2.86	2.67
3	5.24	5.90	2.38	1.90
4	4.29	5.24	2.10	1.43
5	4.10	4.67	2.10	1.43
10	3.81	4.29	2.10	1.43
30	2.67	3.62	1.90	1.43
60	2.38	3.05	1.71	1.43

<sup>a</sup> height of foam column in cm.

Once there is a lack of consensus about a general theory of the foam drainage, the curve fitting using appropriate functions aims at its characterization or better statistical inference. In this context some empirical equations were already proposed to fit such foam decay curves.<sup>20,22</sup> In this work the 4-parameter Weibull equation was chosen after a preliminary comparison with the exponential, logistic, Gompertz, and Morgan-Mercer-Flodin equations (omitted results), which are also able to fit exponential and S-shape curves. For the present purpose, the meaning of the Weibull parameter was interpreted in the following way.



**Figure 3.** Experimental data of foam drainage: (●) SDS, (×) POL, (○) ME and (▲) MSF

Parameter beta ( $\beta$ ) expresses the curve tendency toward S-shape or exponential shape and consequently provides insight into the overall foam behavior in time. The parameter gamma ( $\gamma$ ), indicates the beginning of the liquid drainage process, that means, the lag time. The parameter eta ( $\eta$ ) or scale parameter indicates the position of the function density along the x-axis. Thus, curves with the same  $\beta$  and  $\gamma$  values but different range of x values afforded different values of  $\eta$ .<sup>29</sup> The parameter alpha ( $\alpha$ ) expresses directly the volume of liquid retained in the foam (LVF) at time zero. Mathematically speaking parameter  $\alpha$  is independent of  $\gamma$  and  $\beta$  but induces proportional changes on  $\eta$  (Equation 2).

The fitting parameters calculated according to Weibull and exponential equations for ME, MSF, POL and SDS are showed in Table 2.

**Table 2.** Weibull and exponential parameters calculated for LVF curves (25 ± 2 °C)

Parameter	ME	MSF	POL	SDS
$\alpha$	18.57 (17.22) <sup>a</sup>	19.24 (17.41) <sup>a</sup>	11.43 (10.75) <sup>a</sup>	11.43 (11.21) <sup>a</sup>
$\beta$	-1.04 (-0.404)	-0.99 (-0.349)	-0.81 (-0.627)	-1.81 (-0.683)
$\gamma$	0.57	0.54	0.24	0.42
$\eta$	16.11	16.12	10.11	10.09
R <sup>2</sup>	0.9990 (0.8177)	0.9994 (0.7421)	0.9995 (0.7372)	0.9993 (0.8986)
Std.desv. <sup>b</sup>	0.2877 (2.3142)	0.1949 (2.7303)	0.1173 (1.6914)	0.1634 (1.1282)

<sup>a</sup> Values for the exponential model  $y = \alpha \exp(-\beta x)$  (Potreck, 2004) <sup>b</sup> Regression standard deviation.

Weibull equation was able to fit the drainage curves very well, leading to regression coefficient values above 0.999 in all cases. As a result, the experimental values of LVF at time zero and the calculated values of parameter  $\alpha$  were almost coincident. The parameter  $\alpha$  of ME and MSF was about 2-fold higher than POL and SDS ones. No relationship between parameter LVF and foamability could be assessed by comparing foam height values of ME, MSF, POL and SDS at  $T_0$  (Table 1). The scale parameter indicated that the data density of ME and MSF are placed in a higher right field than POL and SDS, what means, ME and MSF foams stand for a longer time.

All  $\beta$  values calculated are typical of exponential curves<sup>29</sup> but with different negative magnitudes. Since LVF decreases until the system reaches the equilibrium all  $\beta$  parameters were therefore negative. Differently from SDS, the ME, MSF and POL values of  $\beta$  were equivalent. It can be noted an inverse relationship between drainage rate and the respective  $\beta$  magnitudes, but not between the later parameter and the time required for LVF equilibrium (Figure 3).

The values of  $\gamma$  indicate short lag times of about 1 min (ME, MSF and SDS) or even lower (POL).

However, differently of parameters  $\alpha$  and  $\eta$  the statistical comparison of  $\beta$  and  $\gamma$  of each solution assayed seems to be more laborious. The linearization of Weibull equation<sup>30</sup> appears to be feasible, but requires the solving and comparison of four equations simultaneously. The present approach comprises a two-step procedure.

The first step implies the data standardization after parameter  $\alpha$ , taking into account that the other three Weibull parameters are subtracted from it directly (Equation 1). Moreover, the foam capability of each assayed solution is an intrinsic factor and must achieves a maximum value (100%) under controlled experimental conditions. Therefore, all LVF values of ME, MSF, POL and SDS at  $t_0$  can be consider the same and equal to 100% ( $\alpha=100$ ). Under this statement the value of parameters  $\alpha$ ,  $\beta$ ,  $\gamma$  and  $\eta$  were newly calculated (Tables 3 and 4). Obviously, the changing of parameter  $\alpha$  of a given curve alters  $\eta$  but not  $\gamma$  and  $\beta$  as earlier mentioned. Besides that, the regression coefficients remain also unchanged.

**Table 3.** LVF values recalculated after standardization of the initial LVF data

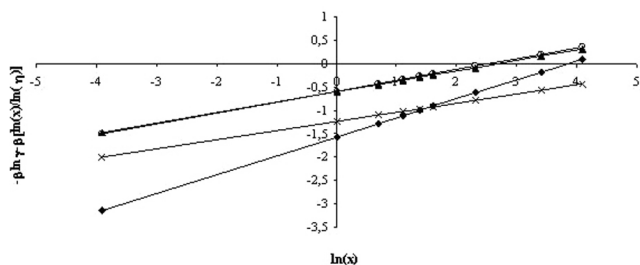
Time (min)	LVF (%)			
	POL	SDS	ME	MSF
0	100.00	100.0	100.00	100.00
1	33.33	41.73	51.29	51.46
2	25.00	23.32	33.32	36.63
3	24.99	16.66	28.19	29.70
4	20.82	12.49	23.07	27.22
5	18.37	12.48	22.07	24.22
10	18.20	12.46	20.51	22.25
30	17.50	12.44	14.37	18.81
60	15.05	12.42	12.92	15.80

**Table 4.** Weibull parameters recalculated after standardization of the LVF data

Parameters	ME	MSF	POL	SDS
$\alpha$	100.02	100.01	100.01	99.99
$\beta$	-1.04	-0.99	-0.86	-1.81
$\gamma$	0.57	0.54	0.24	0.42
$\eta$	86.68	83.66	84.75	88.37
R <sup>2</sup>	0.9990	0.9994	0.9995	0.9993

The second step considers the change of the function density ( $\eta$ ) induced by parameter  $\alpha$ . The right side of Equation 4 encloses the three parameters that describe the variable LVF as a function of time (x). The standardization after  $\alpha$  changed the values of  $\eta$ , but the values of  $\gamma$  and  $\beta$  remained unchanged. Once  $\eta$  express the density of the Weibull function along the x-axis, it seems feasible to cancel out this effect dividing x by respective value of  $\eta$ . By this way a linear relationship can be drawn by plotting  $\ln(x)$  versus  $-\beta \ln(\gamma) - \beta [\ln(x)/\ln(\eta)]$ . After linear regression by the least squares method the slope gives straightforward the value of parameter  $\beta$  and the intercept corresponds to  $\beta \ln(\gamma)$ . The linearized curves by Equation 4 are described in Figure 4.

The comparison of the slopes (parameter  $\beta$ ) demonstrated that the drainage rate, namely LVF decrease, of SDS was the fastest of all, while ME, MSF and POL were statistically not different from each other by the T-Student test (Tables 5 and 6). On the other hand, the statistical comparison of the intercept indicates that the drainage rate and lag time effects were more pronounced for SDS, followed by POL, MSF and ME. Moreover, the difference between slope and intercept of both ME and MSF was not significant.



**Figure 4.** Linearization of Weibull curves from foam drainage: (●) SDS, (×) POL, (○) ME and (▲) MSF

**Table 5.** Values of slope and intercept calculated by linear regression

Coefficients	POL	SDS	ME	MSF
Intercept (a)	1.2346	1.5623	0.5892	0.6059
Slope (b)	-0.8643	-1.8130	-1.0374	-0.9909

**Table 6.** Significance for the slope and intercept according to Student-test (P 0.05)

	T(a)	T(b)
SDS and POL	1.345	9.638 <sup>a</sup>
SDS and ME	3.949 <sup>a</sup>	7.791 <sup>a</sup>
SDS and MSF	4.229 <sup>a</sup>	8.732 <sup>a</sup>
POL and ME	2.525 <sup>a</sup>	1.720
POL and MSF	2.745 <sup>a</sup>	1.368
ME and MSF	0.072	0.496

\* $|T(\text{calculated})| \geq t(0.025; 14) = 1.7613$ . <sup>a</sup>Significant difference at P 0.05

## CONCLUSION

Saponin from mate extract and its purified fraction showed comparable foamability to synthetics sodium dodecyl sulfate and polysorbate 80. The linearization of Weibull function allowed us to determine that the natural surfactants analyzed presented a better performance in terms of foam stability. In addition, it was possible to conclude that ME and MSF, although different in total composition, present the same decay profile.

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